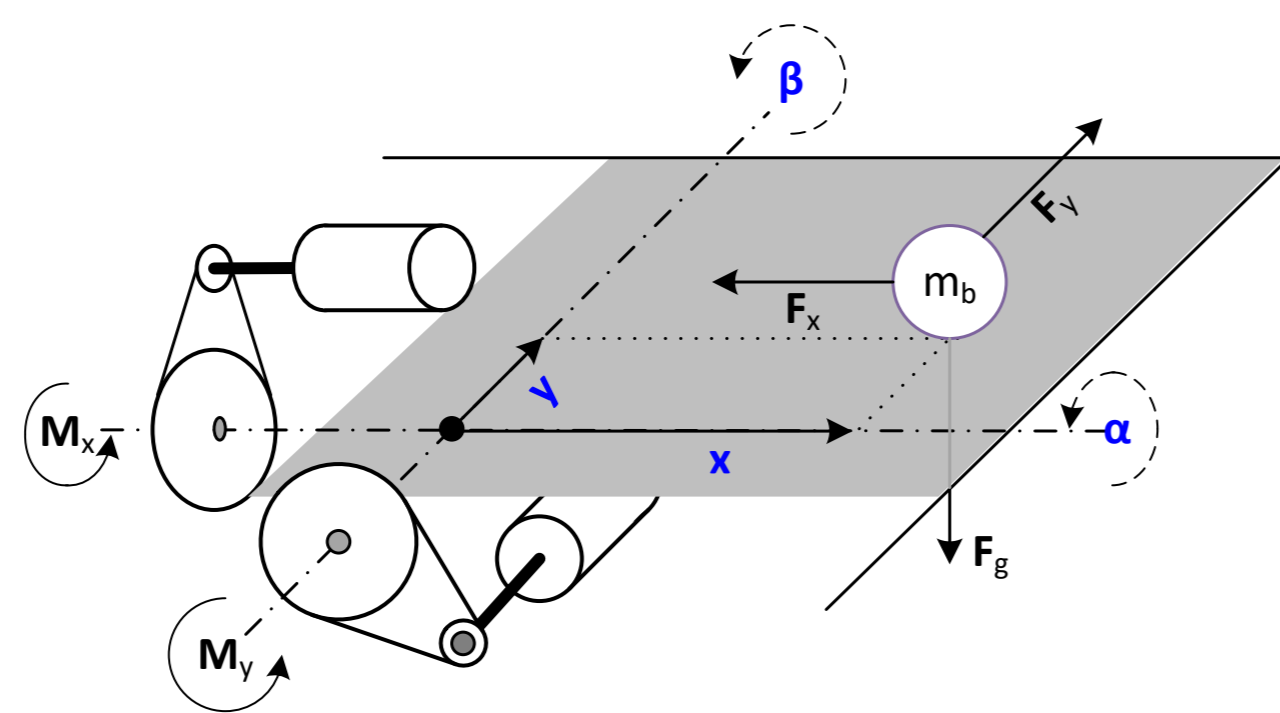


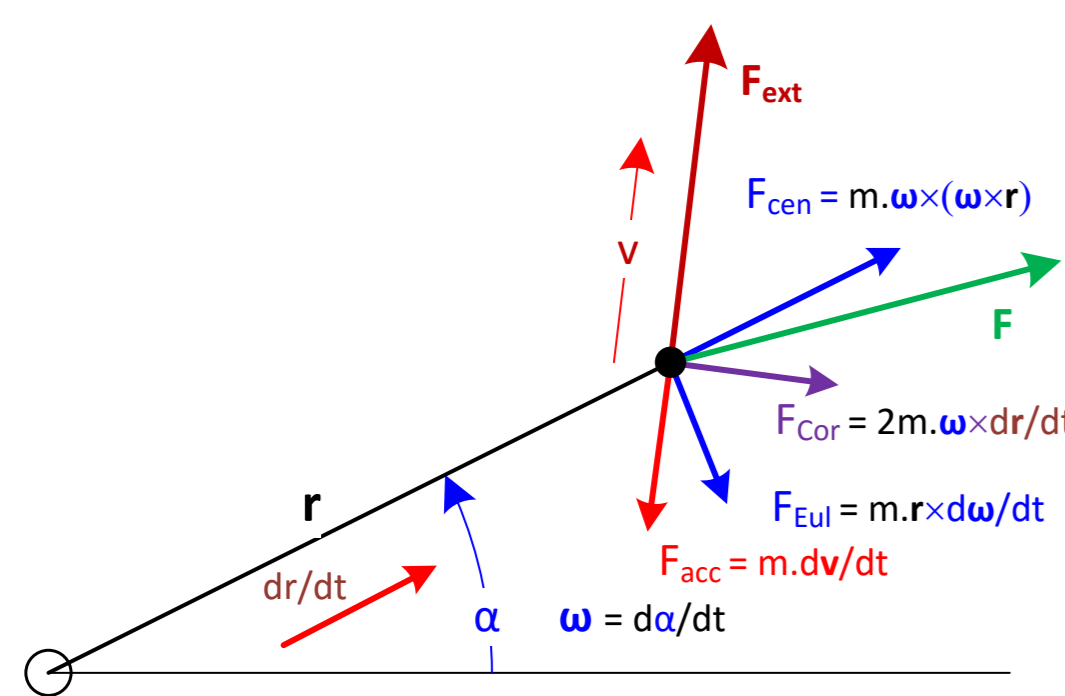
- **Topic** – ball and plate system modelling and optimal control
- **Task** – trajectory tracking of ball and plate system
- **Solution** – modelling of ball and plate system based on first principles by considering balance of forces and torques – by Newton-Euler method. A non-linear model is derived considering the dynamics of the motors, gears and ball and plate. The non-linear model is linearized near the operating region to obtain a standard state space model. The linear model is used for discrete optimal control design – ball is tracked by control voltages of the motors.

## MODELLING (for one axis)

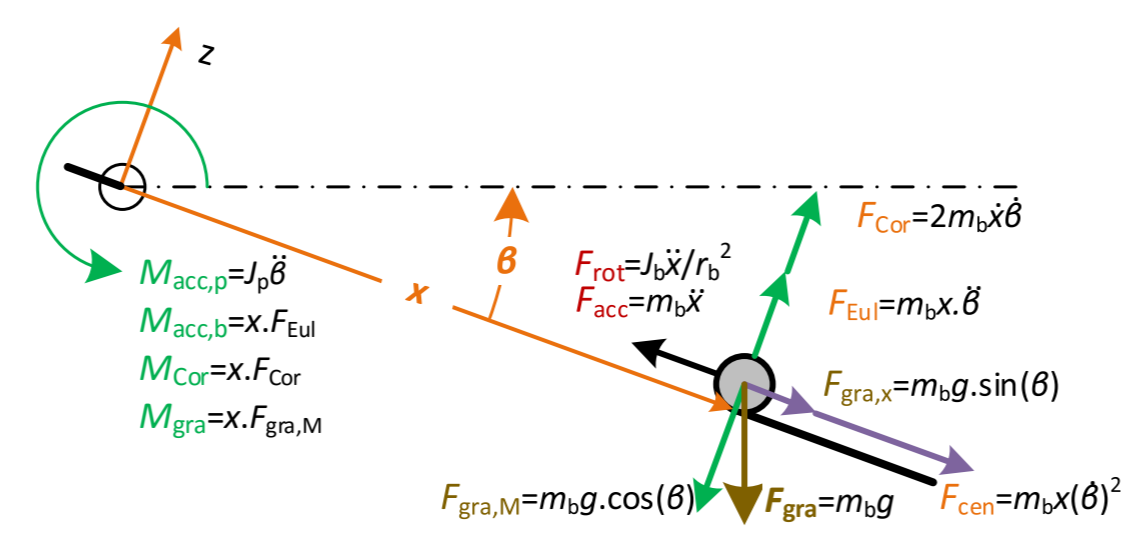


**Balance of forces - ball**  $F_{acc} + F_{rot} + F_{los} + F_{Eul} + F_{Cor} + F_{cen} = F_{gra}(\alpha, \beta)$

$$\left(1 + \frac{J_b}{m_b r_b^2}\right) \frac{d^2 x}{dt^2} + \frac{dx}{dt} \left(\frac{k_b}{m_b r_b} + \frac{k_{cx}}{m_b} \frac{dx}{dt}\right) + x \left(\frac{d\beta}{dt}\right)^2 = -g \cdot \sin(\beta)$$



Forces acting on ball and plate



Movement in the x-axis (x-z plane) and rotation (torque) acting in y-axis

**Balance of moments - plate with ball**

$$M_{acc,p} + M_{acc,b} + M_{Cor,b} + M_{los} = M_{mot} - M_{gra}$$

$$\left(\frac{J_p + J_{Gx}}{m_b} + y^2\right) \frac{d^2 \alpha}{dt^2} + \left(2y \frac{dy}{dt} + \frac{k_{px}}{m_b}\right) \frac{d\alpha}{dt} = \frac{M_{Gx}}{m_b} - y \cdot g \cos(\alpha)$$

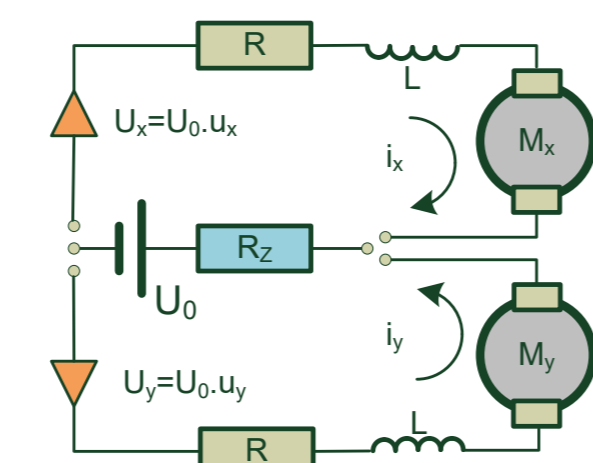
**Gear system**

$$\alpha = \frac{1}{G} \varphi_x, \quad M_{Gx} = G \cdot M_x$$

**Balance of energy and moment – motor**

$$R \cdot i_x + L \frac{di_x}{dt} + k_u \frac{d\varphi_x}{dt} + R_z(i_x + i_y) = u_x \cdot U_0$$

$$J_m \frac{d^2 \varphi_x}{dt^2} + k_o \frac{d\varphi_x}{dt} + M_x = k_m \cdot i_x$$



Equivalent circuit of DC motor

**Final model**

$$a_1 \frac{d^2 x}{dt^2} + \frac{dx}{dt} \left(a_2 + a_3 \frac{dx}{dt}\right) + x \left(\frac{d\beta}{dt}\right)^2 = -g \cdot \sin(\beta)$$

$$(b_{1x} + y^2) \frac{d^2 \alpha}{dt^2} + \left(2y \frac{dy}{dt} + b_{2x}\right) \frac{d\alpha}{dt} = b_3 i_x - y \cdot g \cos(\alpha)$$

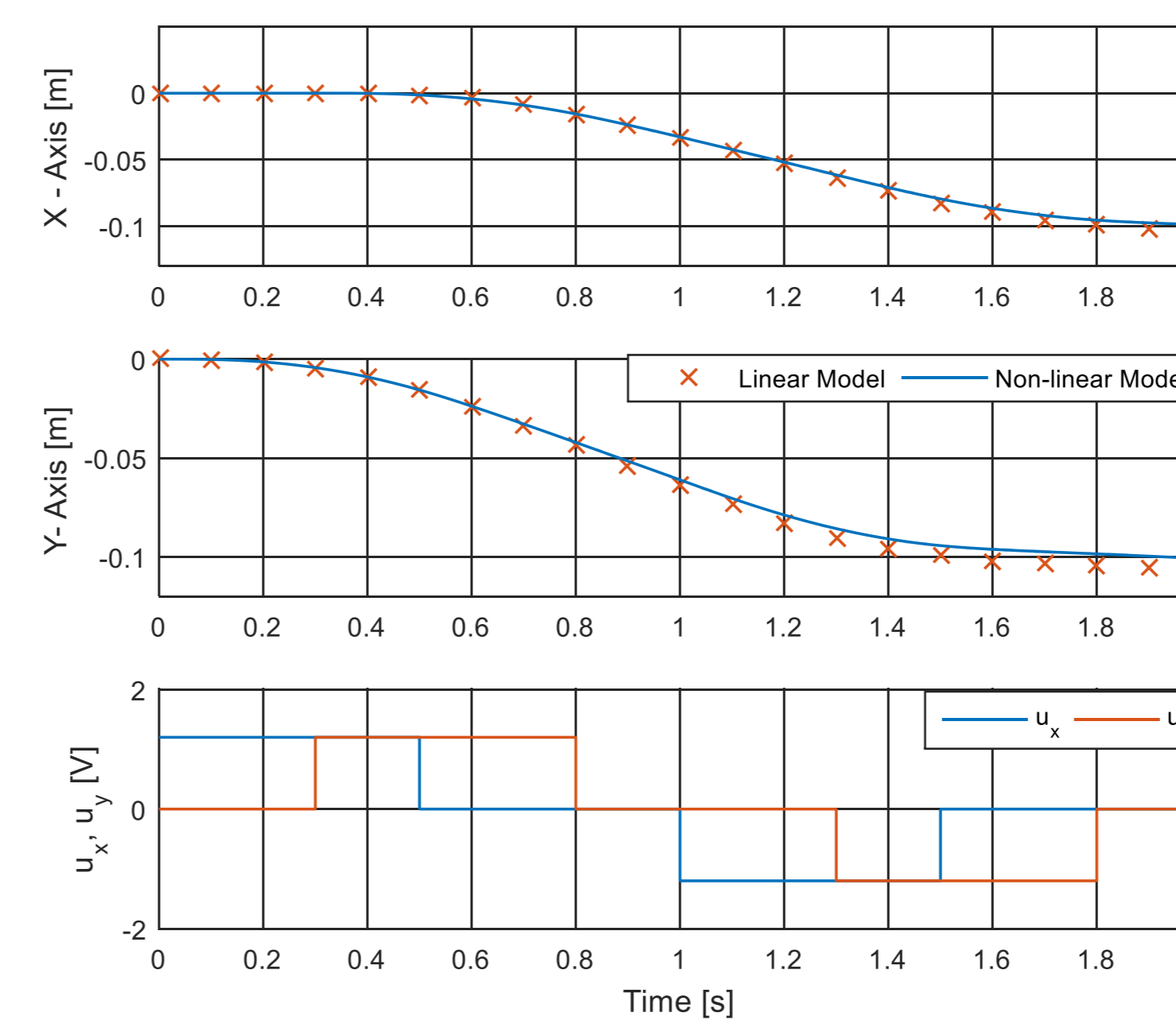
$$\frac{di_x}{dt} + d_3 \frac{d\alpha}{dt} + d_2 i_x + d_1 i_y = d_0 u_x$$

## LINEAR STATE SPACE MODEL

$$\frac{d\bar{x}}{dt} = \bar{A}\bar{x} + \bar{B}u$$

$$y = \bar{C}\bar{x}$$

$$\bar{x} = [x \quad v_x \quad \alpha \quad \omega_x \quad i_x \quad y \quad v_y \quad \beta \quad \omega_y \quad i_y]^T$$



Outputs and inputs in open loop verification

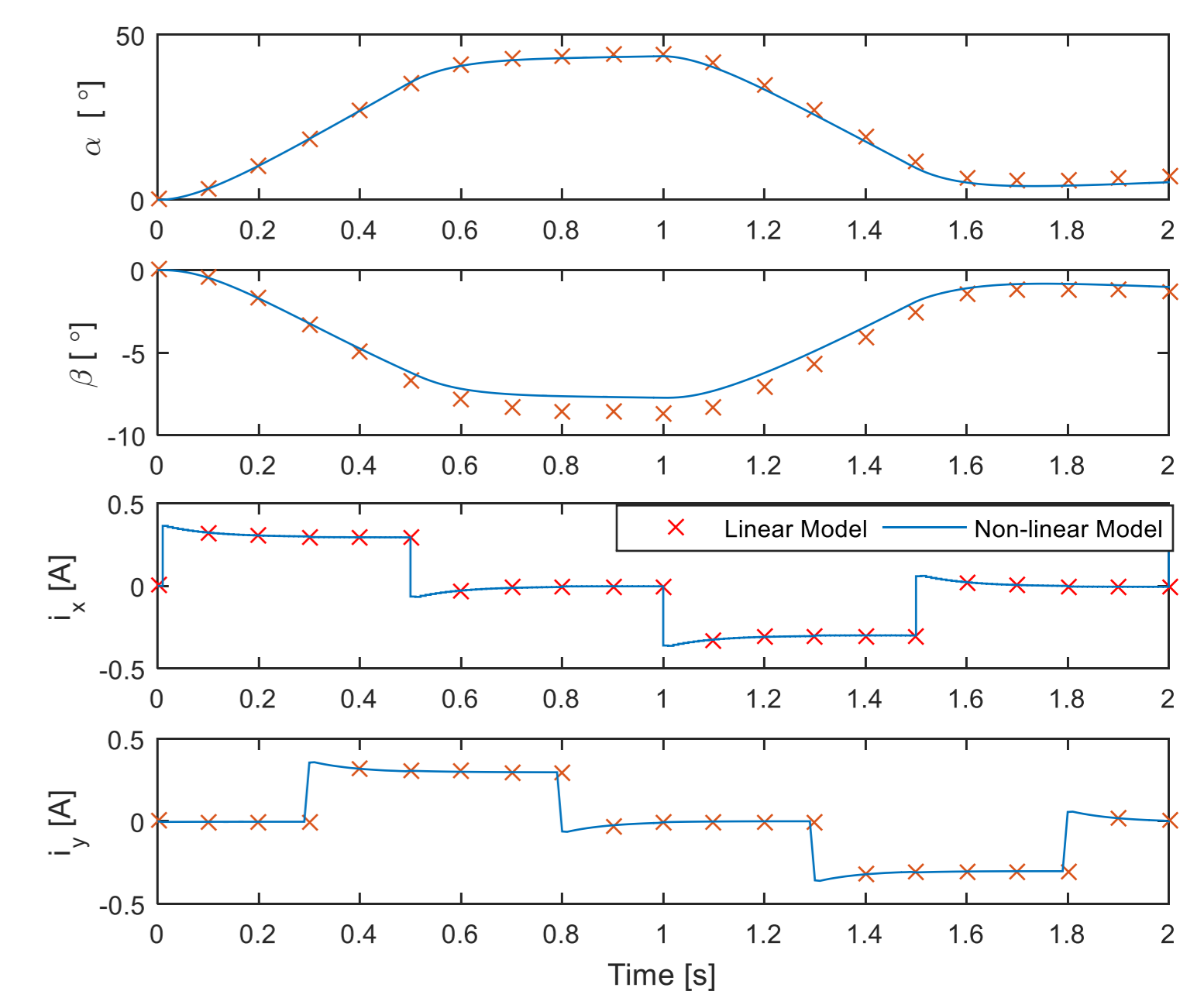


Plate angles and motor currents in open loop verification

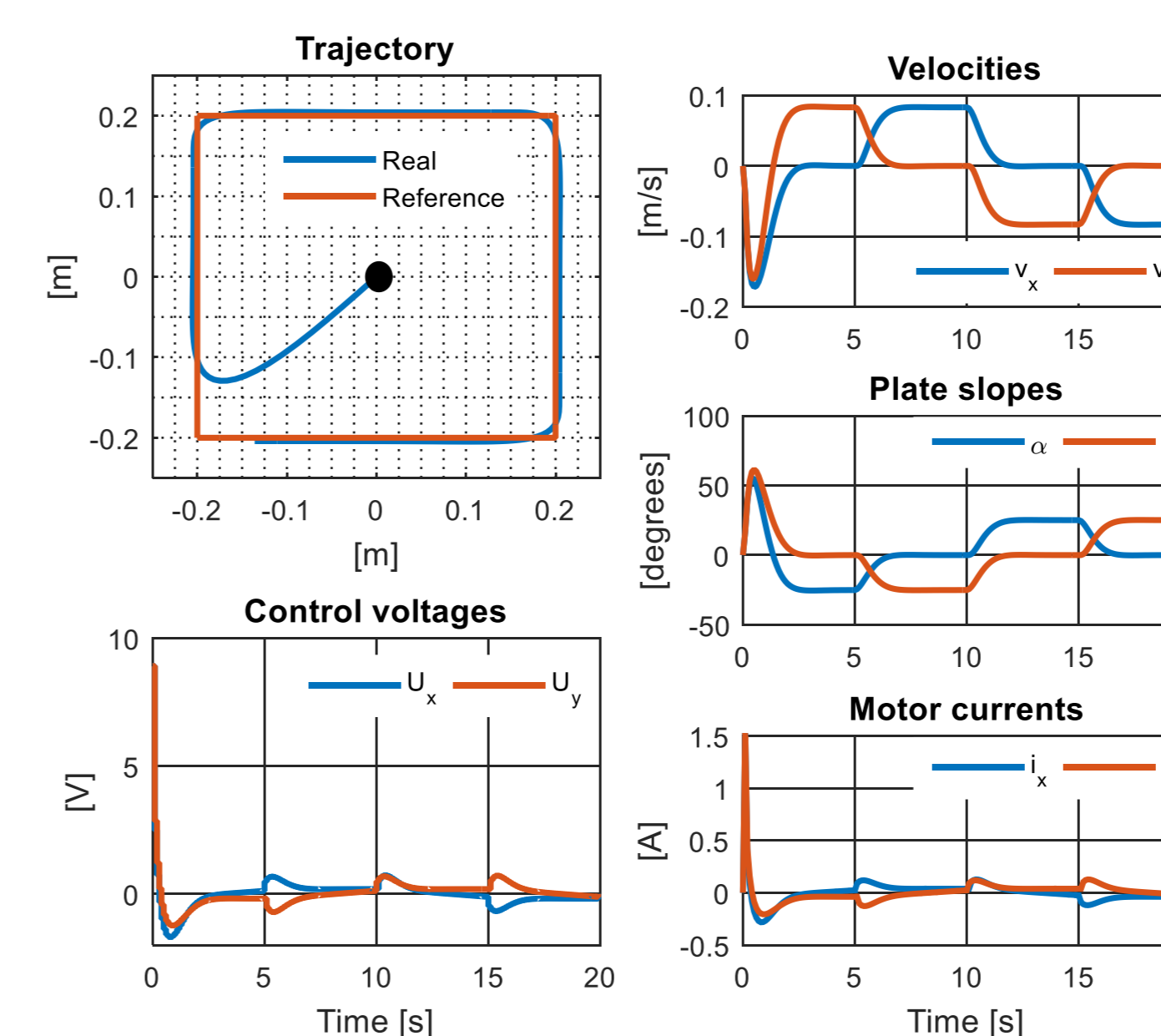
## OPTIMAL CONTROL

$$\mathbf{x}(k+1) = \mathbf{A}\mathbf{x}(k) + \mathbf{B}\mathbf{u}(k)$$

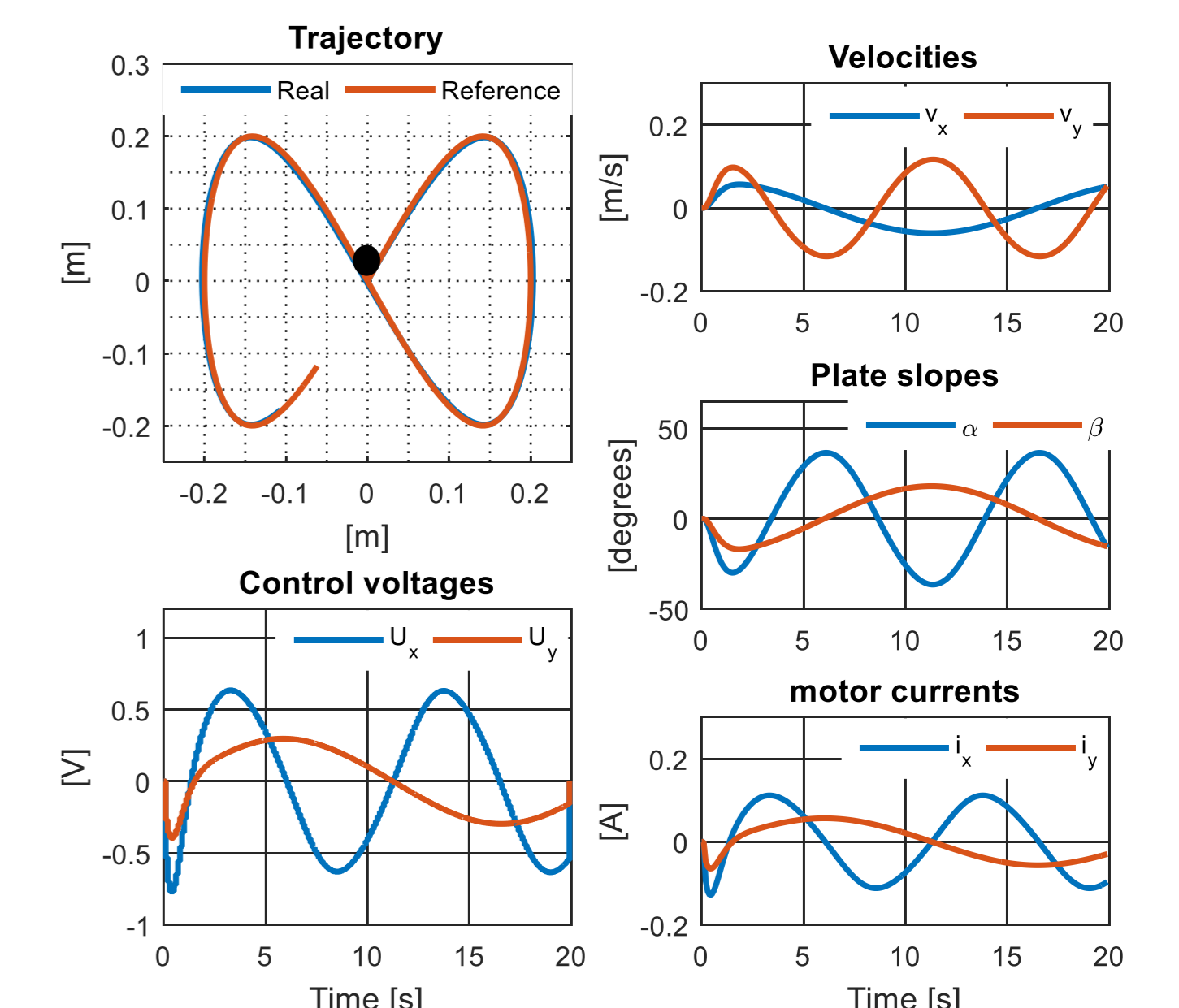
$$\mathbf{y}(k) = \mathbf{C}\mathbf{x}(k)$$

$$J_\infty = \sum_{i=1}^{\infty} [\mathbf{x}^T(k+i)\mathbf{Q}\mathbf{x}(k+i) + \mathbf{u}^T(k+i)\mathbf{R}\mathbf{u}(k+i)]$$

$$\mathbf{u}(k) = -\mathbf{K}[\mathbf{x}(k) - \mathbf{x}_w(k)]$$



Square trajectory tracking



Lissajous curve trajectory tracking